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DESIGN STUDY FOR A HIGH ENERGY MUON BEAM

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INTRODUCTION

Plans for upgrading the muon physics program at Fermilab have been under discussion for several years and typically focus on an improved muon beam. The Fermilab Summer Study Reports for 1968, 1969, 1970, 1973, 1976 all have papers and discussion on this topic. The last named study stimulated a detailed design project by the authors on which we report in this document. The general guideline we adopted in this work was to create a new muon beam design appropriate to the Tevatron era at Fermilab (1000 GeV protons). The design was further constrained to yield good performance at present lower proton beam energies (400 GeV). Within this context, we applied the following design criteria:

- i) high efficiency ($\mu / p \sim 10^{-5}$)
- ii) low "halo" (halo/beam $\sim 5\%$)
- iii) broad tuning range ($275 \leq p \leq 750$ GeV)
- iv) good optical quality ($R_{beam} \leq 3$ cm)
- v) low hadron contamination ($\pi/\mu < 10^{-6}$)
- vi) freedom from interference with other beams and equipment
- vii) momentum tagging capability ($\Delta p/p \leq 2\%$)
- viii) acceptable radiation hazard on-site and at site boundaries.

This preliminary study of several beams along with their associated halos has been done using the Monte Carlo programs DECAY TURTLE⁽¹⁾ and HALO.⁽²⁾ The CERN-SPS muon beam design expects to realize a halo/beam ratio of $\sim 2\%$ over 4x4 meters⁽³⁾; our definition of halo corresponds to a 10 foot x 10 foot area.

PROTON BEAM

The overall plan for achieving a proton beam and production target for muon experiments separate from the existing N0 beamline is shown in Figures 1 and 1a. The essential features are taken from TM729⁽⁴⁾ (alternative 2) with minor modifications. The path of the beam is 30 milliradians to the east and 10 feet below the N0 beamline. The main points of the proposal are:

- 1) The existing G line is split horizontally with 50 ft. of electrostatic septa at the G1 manhole.
- 2) A new tunnel section labeled G1.5 will contain 60 feet of Lambertson magnets which bend vertically.
- 3) G2 will be extended and contain four 22 foot superconducting dipoles run at ~ 40 kilogauss. The dipoles will be rotated so that they complete the 10 milliradian vertical bend started by the Lambertsons, and give a horizontal bend of 30 milliradians.
- 4) The beam drifts to the Muhall target areas in the vicinity of Enclosure 100 where it is focussed onto the target.
- 5) The majority of the new beamline can be installed by means of a trenching and pipe burying operation. Since the beam is 10 feet underground, little earth moving will be required for berm construction. There is no interference with Nuhall, the Target Service Building, or modifications to the decay pipe. No penetration of the Neutrino "bathtub" for containing radioactive ground water is necessary nor is any digging of radioactive soil.

THE MUON BEAM

The muon beam basically consists of two target stations, a front end triplet which efficiently collects the parent particles, a decay section, a hadron absorber, and a part which selects and tags muon momenta and reduces halo. We have mainly employed the WANG⁽⁵⁾ parameterization of particle yields with the standard assumption of $K/\pi \approx 0.1$. An alternative

parameterization which makes a definite prediction for the K/π ratio at high energies is that due to Adair⁽⁶⁾. The pion yields matching to the acceptance of the proposed beams are compared for these two parameterizations in Table I. The WANG pion yields are about twice those of Adair. Adair predicts a larger K/π ratio than the 10% usually assumed.

In order to check these formulae, we have attempted to reproduce the muon yields in the existing muon beam at Fermilab (N1 line). We have used the WANG parameterization, but can scale to the Adair prediction using the pion yields of Table I. The yields are computed using HALO for 150 and 225 GeV/c operation. The targeting angle of the primary proton beam onto the target (with respect to the N1 beamline direction) was 0.3 mr and 0.7 mr, respectively,⁽⁷⁾ which required a small modification to be made to the HALO subroutine PIGEN where zero degree targeting and production are assumed. The differences from the zero degree values were <10%. As is seen from Table II, the predictions are in reasonable agreement with the measured yields. The geometry of the N1 beamline assumed in HALO is given in Appendix I.

Four different beam configurations have been considered, although only the two having the best halo to beam characteristics were modeled in detail. For completeness, we give all four beam layouts and note that three of these (called 1-3) have a common front end, Figure 2a, while the fourth is different, Figure 2b. The primary features of each section are described below. The design uses the specifications of an existing quadrupole, the 4QL20⁸, and 20 foot long, 15 kilogauss bending magnets with 4"x6" aperture.

A. Target Stations

The proton beam will be directed at either of two targets in Muhall. The two targets will be separated in Z by 24 feet.

The upstream target will be used whenever the pion beam is tuned for a momentum greater than 600 GeV/c. Using this scheme the triplet will capture roughly the same p_{\perp} at high and low energies. These two targets could be placed in two

separate manholes similar to the target manhole that now exists in the decay pipe. It is also possible that a target tube similar to that in Nuhall could be used. One train car containing the target, a collimator and the necessary instrumentation should suffice. The cost of the target tube with its associated tracks and access tunnel is comparable to the cost of the manholes. The manholes offer the advantage of having vacuum all along the beam, however servicing and repairing take longer.

B. Hadron Capture Section

The purpose of this front-end quadrupole triplet section is to collect as many pions and kaons from the target in as large a momentum band as possible. A fifteen foot water-cooled collimator will be placed immediately downstream of the target to absorb low energy/wide angle parent particles. This will be followed by a triplet consisting of ten quadrupoles aligned at zero degrees with respect to the incident proton beam. The configuration is the same at 750 and 550 GeV/c; two quadrupoles and a drift space are interchanged for the 275 GeV/c operation. Beams 1-3 contain bending magnets in a notch arrangement serving to get rid of the low energy/wrong sign parent particles. All particles greater than 0.6p are transported, dispersion-free, to the end of the decay channel where there is a water-cooled beryllium absorber. When the channel is tuned for parent momenta ≥ 600 GeV/c, the 1000 GeV diffracted proton beam is carried along the channel and is dumped at the beryllium absorber. At lower energies the 1000 GeV beam will encounter a conventional dump in the notch. The FODO channel, when tuned for 275 GeV/c muons, cannot transport the diffracted proton beam without significant losses. Beam 4 dumps the protons at the front end and the dipole bending selects $\pm 10\%$ $\Delta P/P$. This eliminates early in the beam some of the particles contributing

to the halo at the end of the beamline. The dispersion at the momentum slit of Beam 4 is shown in Figure 3. Note that there is no horizontal focus at the momentum slit, unlike the CERN beam, but the triplet delivers a parallel beam to the decay FODO. This selection slightly reduces the muon yield as compared to Beams 1-3. These are summarized in Table III.

C. Decay Channel (π/K Decays)

The criteria for obtaining the highest possible muon flux per proton have been variously described.⁽⁹⁾ As illustrated by the CERN design, the FODO array provides the most efficient transport system allowing pions from a wide momentum band to contribute muons to the desired momentum interval.

The decay channel is a FODO array composed of 4Q120 quadrupoles having an average half-aperture of 2.25 inches. The efficiency of the channel as a function of particle momentum is shown in Figure 4. This curve was made with the FODO tuned to maximize the muon flux from parent particles of central momentum P . The transmission of the beamline was studied using the program DECAY TURTLE, modified to input a parent production spectrum. The results of keeping the decay length constant and removing magnets in the Parent FODO are shown in the following table.

PARENT FODO		MUON FODO	RELATIVE μ / p TRANSMISSION		
L(feet)	No. of Magnets	L(feet)	800	305	(GeV/c)
200	15	200	1.00	1.00	
326	10	200	0.47	0.41	
550	6	200	0.41	0.30	
3370	0	200	0.08	0.06	
(parallel beam)					
326	10	326	0.9	0.8	
143	21	143	1.03	1.12	

After removing the magnets the channel was tuned for maximum muon flux while being constrained to match into the Muon FODO. The quadrupole strength and hence the phase advance per period is arranged so as to contain with minimum losses the parent beam of central momentum P and a wide momentum band of muons resulting from their decay. One can obtain a better transmission at the expense of a) adding additional matching sections to take the beam from the Parent FODO, make a small beam spot on the beryllium plug, and then match into the Muon FODO, or b) making the distance between quadrupoles, L , the same for both FODO's. The first option is not very attractive because the number of magnets required for the matching sections is comparable to the number removed from the Parent FODO. The second alternative has the drawback of increasing the total length and thus increasing the distance that the utilities have to be extended. In going from $L=200$ feet to $L=326$ feet, the length of the Muon FODO increases from 1470 feet to 2350 feet. This distance could be reduced somewhat by increasing the phase advance per period in the Muon FODO, but would save only one magnet and correspondingly only 326 feet. Taking out more magnets would mean that the angular dispersion, $d\theta/dp$, would be non-zero. The maximum field strength of the 4Q120 gives a minimum value for L of 140 feet, and has been included in the table for completeness. We have chosen to study in detail beams with $L=200$ feet for both FODOs. Use of a phase advance of ~ 60 degrees per FODO period for all momenta yields both good transmission and a reasonably small spot size at the beryllium absorber so multiple scattering can be minimized. In this way the absorber can be located within the FODO without additional matching sections. Typically, only a small part of the

halo at the end of the beam originates in the decay channel, as shown by Figure 5.

D. Muon Transport Section

At the end of the decay section and the beginning of the final FODO section is a hadron absorber which reduces the π/μ contamination at the end of the beam to $<10^{-6}$. The absorber, ~ 35 feet of beryllium, is located immediately downstream of the last quadrupole of the decay channel and inside the first dipole of the Muon FODO. This will also serve as the primary proton dump when the beam is tuned for high energy positive muons. Following the absorber the first bending magnet selects the desired muon momentum band. Optically this is followed by a continuation of the Parent FODO. The four beams differ in the number of FODO periods used to transport the beam from the absorber to the detector and in the direction of bending, as shown in Figures 8a, 8b, and 8c. In the case of Beam 4, we have simply used the same muon FODO as for Beam 2. Most halo at the experiment originates after the absorber, and Beam 2 is found to have the best halo to beam characteristics. It is envisaged, when desired, that momentum tagging of individual muons entering the detector can be accomplished by following the trajectories through the last dipole, using MWPC's and scintillation counters. The muon yields at the detector for beams 2 and 4 are given in Table III. Three complete periods are used to rotate the phase space by 180 degrees. The final bending magnet, in the same direction as the first, is placed to cancel $d\theta/dp$. Halo removal is accomplished by a series of magnetized iron pipes and toroids.

E. Halo

The halo considerations can be separated into two parts. There is the direct question of how many muons accompany the beam into the detector, and also how many muons irradiate the outside

world. We have been particularly concerned with reducing the former, although we have also estimated the latter. As noted in the 1976 Summer Study⁽¹⁰⁾, the halo muons are best removed by interposing magnetized iron to deflect them away from the beam. The elements introduced are iron toroids (at magnetisations of 15 kg) and sections of magnetized iron beam pipe (this mupipe is described in Appendix III). The mupipe introduces a hard magnetic edge close to the extreme excursion of the beam; we use a pipe with internal and external radii 2 and 3 inches, respectively. The radial dimensions were varied in the study and the criticality of the alignment was estimated. These are followed at strategic places with large magnetic toroids placed so as to intercept the halo deflected out by the mupipe and thus clear out the larger area. There are two toroid sections, one 4 feet and the other 3 feet in radius. Both are 40 feet long with a 3 inch radius hole.

The initial deflection of the unwanted muons is started by the mupipe, and then increased further by the large toroids. This halo distribution at the detector, before any attempt is made to deflect halo from the beam direction, is shown in Figure 6 for Beam 2. We assume the detector would present a cross section not larger than 120" x 120". However, in order to have a clear working space, we also define an area of 300" x 200" about the beam. This consideration was used to fix the lengths of the magnetized Toroids.

Program HALO will indicate where in the beam line the offending muons left the aperture and became halo (see Figure 5 for the beam without magnetic scrapers). This helps in placing the iron. The scrapers we have considered are labelled in Figures 8 (a, b, c). We started off by assuming a 1" wall, 4" ID mupipe with 5 ft. radius, 40 ft. long toroids. The halo/beam ratios resulting for various combinations of these elements are given in Table IV.

From this we have selected beams 2 and 4 for further study with all of the magnetic scrapers shown in Figure 8 included in both cases. Note, we have accepted the program decision that once a muon has hit an aperture it is labelled halo. There remains the possibility of accepting the beam-like halo, i.e. halo close to the real beam, as beam provided it is tagged satisfactorily.

We find that use of a 2" thick beam pipe wall for the first section of mupipe requires a larger toroid, and have settled on 1" thick wall with 4 ft. and 3 ft. radii, respectively, for the upstream and downstream toroids. For Beam 2, we show in Table V the halo/beam ratio with the final scrapers and the triplet and FODO tuned to various muon momenta. The halo is rather constant as the beam momentum decreases.

In order to check the credibility of the HALO results, we have attempted to model the N1 beam/halo situation. With the geometry assumed in Appendix I, Table II compares the halo/beam predictions at both 150 and 225 GeV/c with the observed values. Note that the magnet maps were rough approximations in the case of most of the N1 beam quads; the situation was better for the bending magnets. The 150 GeV/c results are for 300 GeV protons on target. There is reasonable agreement between prediction and measurement.

F. Further Considerations

The low halo-to-beam ratio obtained using the mupipe idea is clearly dependent on introducing the field as close as possible to the beam envelope. We have studied the sensitivity of the result to misalignment by randomly displacing the four sections of mupipe with results shown in Table VI. Clearly the halo and even the muon flux are hurt if misalignments exceeding 1/4" are introduced.

The effect of quadrupole misalignments was studied, and in general the further upstream the misalignment and the lower the momenta, the worse the transmission. Since most of the upstream section of the triplet is running with the quads at full strength, alignment becomes very critical at 275 GeV/c. Misalignments of 0.1" and 0.25" on the two quads running at -5.5 kg/in. reduce the flux at the muon lab by factors of 0.83 and 0.09 respectively at 275 GeV/c. A 0.25" misalignment at 800 GeV/c in these same quads yields a 0.93 reduction factor.

As shown in Figure 9 for Beam 2, there is no strong correlation between the parent decay angle and the muon momenta. However, there is significant polarization information preserved in Beam 4 (see Figure 10) at the expense of intensity.

At the vicinity of the Muon Lab, the angles of the beam, θ and φ , are small. This means that either a long hydrogen target or a stacked solid target could effectively be used. The muon fluxes at ground level at the location of the site boundary were estimated using HALO, and indicate a maximum radiation level of about 40 mrem/yr., assuming 10^{13} protons on target, and 365 days of operation at a Doubler cycle of 60 seconds. More realistic expectations for annualized total operating times and targetted proton intensities will reduce this level to the order of 10 mr/yr.

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Table I
Yield Per 10^{12} Interacting Protons in Hydrogen

	Wang	Adair
π^+ { 400 GeV Protons 0 - 400 GeV/c 0 - 20 mrad	1.07×10^{12}	3.35×10^{11}
π^+ { 400 GeV Protons 175 - 400 GeV/c 0 - 20 mrad	3.36×10^{10}	1.53×10^{10}
π^+ { 400 GeV Protons 200 - 400 GeV/c 0 - 5 mrad	1.87×10^{10}	5.81×10^9
π^+ { 300 GeV Protons 120 - 300 GeV/c 0 - 5 mrad	3.79×10^{10}	1.35×10^9
π^+ { 1000 GeV Protons 350 - 1000 GeV/c 0 - 10 mrad	6.82×10^{10}	3.12×10^{10}
K^+ { 1000 GeV Protons 350 - 1000 GeV/c 0 - 10 mrad	6.82×10^9 ⁺	7.86×10^9
* π^+ { 1000 GeV/c Protons 380 - 1000 GeV/c 0 - 1.5 mrad	2.18×10^6	9.34×10^5
* K^+ { 1000 GeV/c Protons 380 - 1000 GeV/c 0 - 1.5 mrad	2.18×10^5 ⁺	2.02×10^5

⁺ Assume $K/\pi \sim 0.1$.

^x Corresponds approximately to acceptance N1 beam.

* Corresponds to acceptance of Beams 1-4 at 800 GeV/c.

Table II

The Predicted (Wang) and Measured Beam and Halo Rates
 for the N1 Beam Normalized to 10^{12} Incident Protons on
 One Interaction Length Target [obtained by multiplying thin
 target yields in hydrogen by 0.37] .

Beam Tune GeV/c	Type	Predicted Muon Yield μ/p		Measured Muon Yield	Predicted Halo* Beam	Measured Halo Beam
		π^+	K^+			
150	Beam	$(2.96 \pm 0.52) 10^{-7}$		1.7×10^{-7}	4.7 ± 1.9	1.5
	Halo	$(1.4 \pm 0.5) 10^{-6}$				
225	Beam	$(5.2 \pm 0.4) 10^{-7}$	$(0.86 \pm 0.23) 10^{-8}$	2.5×10^{-7}	1.3 ± 0.5	1.9
	Halo	$(7.3 \pm 2.3) 10^{-7}$	$(0.37 \pm 0.37) 10^{-7}$			

*Defined as coincidence between scintillator planes as in the experiment.

Table III
Muon Yields at End of Beam for Given Tune per Interacting
Proton in Hydrogen Expressed as μ/p

Beam and Tune	Δp^*	Wang Muon from π^+	Δp	Adair Muon from K ⁺
No. 2 750 GeV/c	670 \pm 70	$(1.06 \pm 0.08) 10^{-5}$	715 \pm 99	$(0.13 \pm 0.04) 10^{-5}$
No. 2 550 GeV/c	510 \pm 63	$(0.88 \pm 0.03) 10^{-4}$	546 \pm 62	$(0.06 \pm 0.01) 10^{-4}$
No. 2 275 GeV/c	264 \pm 37	$(2.96 \pm 0.10) 10^{-4}$	266 \pm 25	$(0.06 \pm 0.01) 10^{-4}$
No. 4 750 GeV/c	—	$(4.6 \pm 1.3) 10^{-6}$	—	—
No. 4 550 GeV/c	550 \pm 60	$(3.0 \pm 0.1) 10^{-5}$	—	—
No. 4 275 GeV/c	263 \pm 31	$(1.5 \pm 0.06) 10^{-4}$	—	—

* Standard Deviation.

Table IV

Halo/Beam Ratio for Various Scraper/Toroid Configurations.
All for 800 GeV/c Tune per Interacting Proton in Hydrogen

Beam	Magnetic Configuration	Beam Muons μ / p	Halo Beam
1	None	$(1.0 \pm 0.2) 10^{-5}$	11
2		$(8.37 \pm 1.0) 10^{-6}$	10
3		$(6.8 \pm 1.4) 10^{-6}$	9.5
2	(S1, S3; T1, T2)	$(8.37 \pm 1.0) 10^{-6}$	~ 0.5
3		$(6.8 \pm 1.4) 10^{-6}$	~ 0.5
1	(S1, S2, S3, S4; T1, T2)	$(7.6 \pm 1.4) 10^{-6}$	~ 1.0
2		$(8.37 \pm 1.0) 10^{-6}$	~ 0.1
3		$(6.3 \pm 1.3) 10^{-6}$	~ 0.5
4		$(4.6 \pm 1.3) 10^{-6}$	~ 0.1

Table V
Halo/Beam Ratio for Beam 2 per Interacting Proton in Hydrogen
 (Statistics for 15,000 π^+ , and 5,000 K^+)

Parent Particle and Momentum (GeV/c)	Muon Yield μ/p	Halo μ/p	Halo Beam
800 π^+	$(1.06 \pm 0.08) 10^{-5}$	$(0.52 \pm 0.21) 10^{-6}$	9%
800 K^+	$(0.13 \pm 0.04) 10^{-5}$	$(0.4 \pm 0.2) 10^{-6}$	
600 π^+	$(0.88 \pm 0.03) 10^{-4}$	$(2.5 \pm 1.1) 10^{-6}$	4%
600 K^+	$(0.06 \pm 0.02) 10^{-4}$	$(1.0 \pm 1.1) 10^{-6}$	
305 π^+	$(2.96 \pm 0.10) 10^{-4}$	$(2.0 \pm 0.4) 10^{-5}$	7%
305 K^+	$(0.06 \pm 0.02) 10^{-4}$	---	

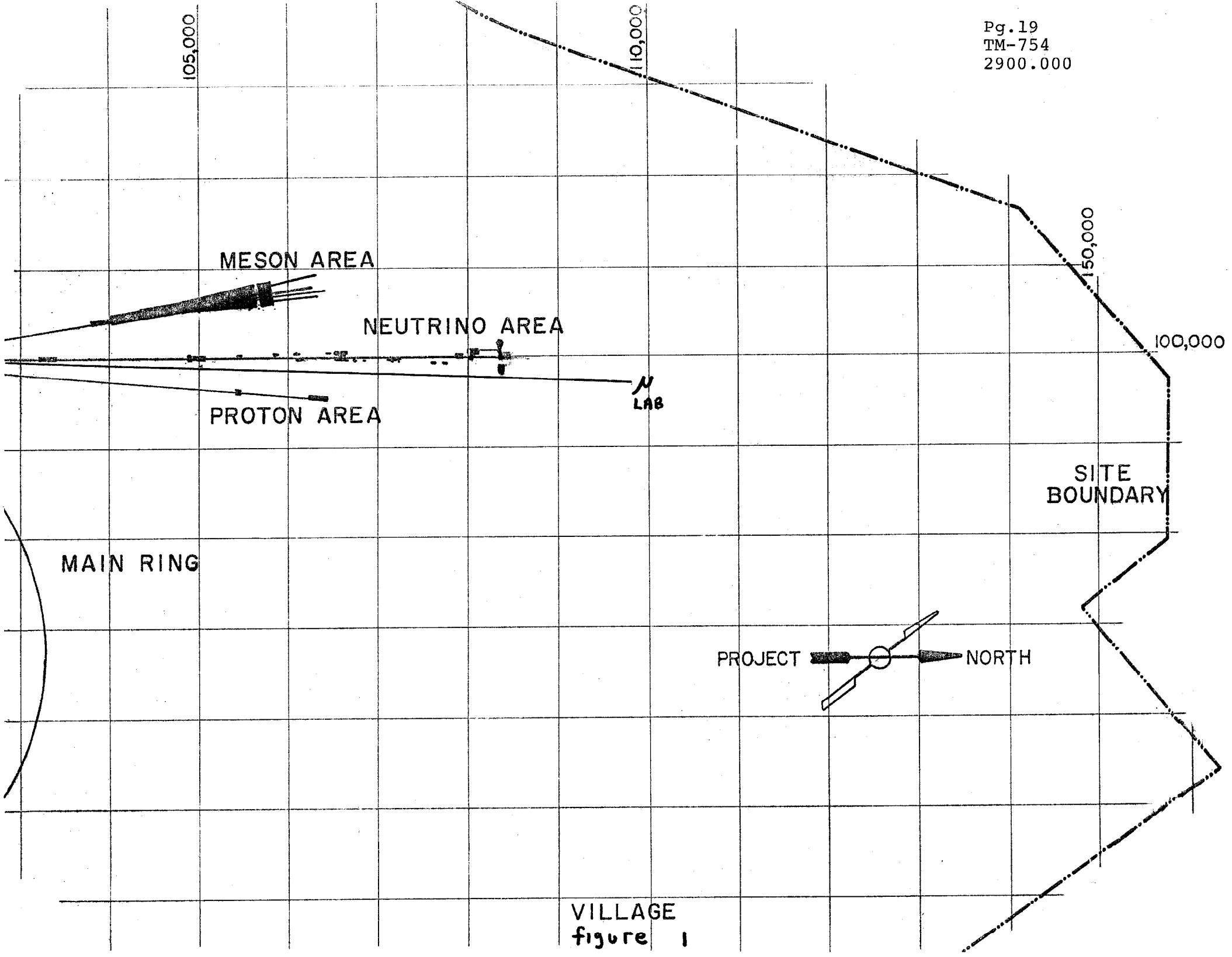
Table VI

The Effects of Mu-Pipe Misalignments for Beam 2.
 (Yields are per interacting proton in hydrogen.)
 Beam Tuned for 550 GeV/c.

Magnitude of Random Pipe Translation (Inches)	Muon Yield μ / p	Halo Beam (%)
0.0	$38 \pm 0.03) 10^{-4}$	2.8 ± 1.2
0.25	$(0.3 \pm 0.6) 10^{-5}$	4.4 ± 1.7
0.50	$(4.5 \pm 0.05) 10^{-5}$	7.7 ± 3.0

FIGURE CAPTIONS

- Figure 1 Layout of the new muon beam.
- Figure 1a Layout of the new muon beam.
- Figure 2a The front end and decay channel for Beams 1-4.
- Figure 3 The momentum dispersion at the momentum slit of Beam 4 at 275 GeV/c.
- Figure 4 FODO transmission as a function of tune momentum.
 p = the central momentum of the parent particles.
- Figure 5 The longitudinal points of origin for halo muons inside a 120" radius area at the end of Beam 2.
- Figure 6 The halo, defined as muons which have left the beam aperture, with no magnetic scrapers.
- Figure 7 The halo with all scrapers on.
- Figure 8 The back end (Muon FODO) for Beams 1-4.
- Figure 9 The momentum of the muon beam at the detector versus the decay angle of the parent pions for Beam 2.
- Figure 10 The momentum of the muon beam at the detector versus the decay angle of the parent pions for Beam 4.
- Figure 11 The x distribution of the muon beam at the detector.
- Figure 12 The y distribution of the muon beam at the detector.
- Figure 13 The p distribution of the muon beam at the detector.



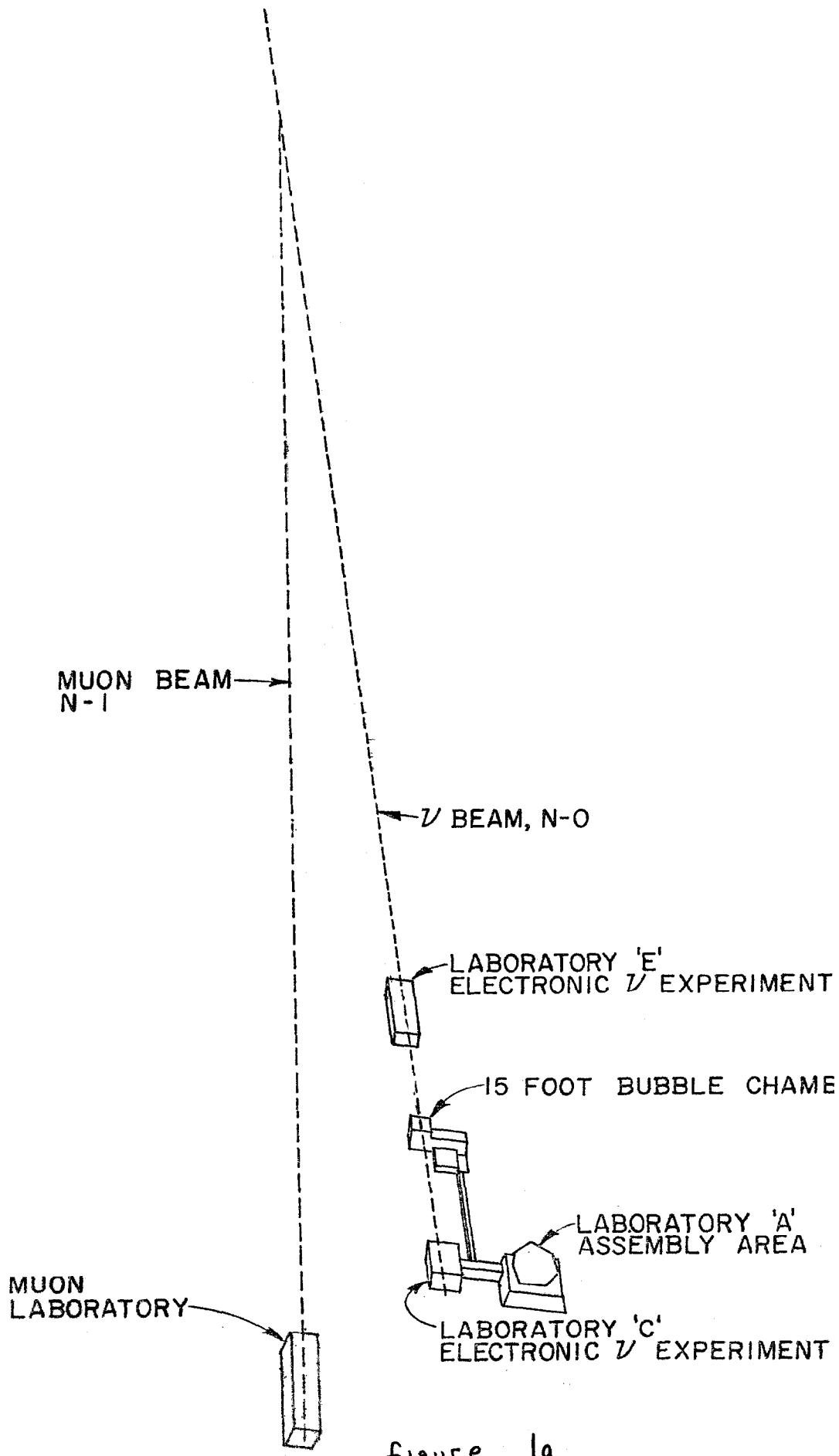


figure 1a

fig. 2a

FRONT END FOR BEAMS 1-3

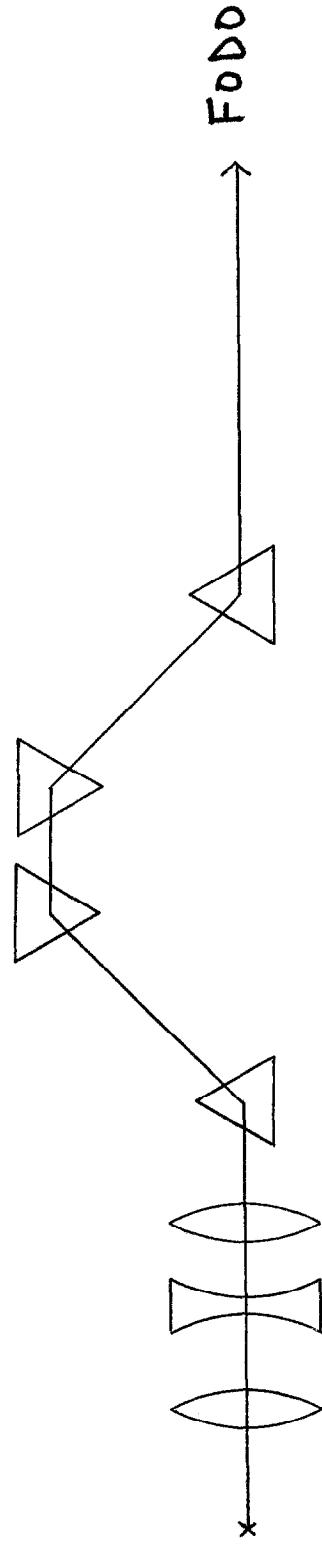
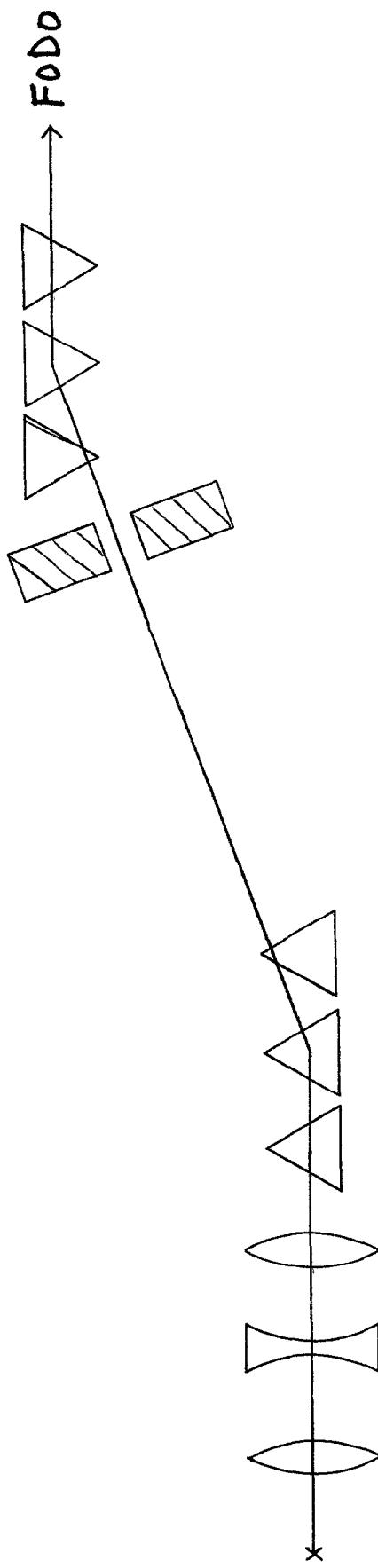


fig. 2 b

FRONT END FOR BEAM 4



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HISTOGRAM NO. 1				DATE 09 OCT 77		TIME 00,08,35		PAGE 15			
HORIZONTAL AXIS... X		IN IN	FOR PI	AT	285,972 FT	(POSITION NO. 28)					
VERTICAL AXIS... P		IN GEV/C	FOR PI	AT	285,972 FT	(POSITION NO. 28)					
		-4.00	1.00								
				SUMS							
200,000 TO	220,000	X8				87					
220,000 TO	240,000	ISV				1029					
240,000 TO	260,000	ISSSSSI				1450					
260,000 TO	280,000	XSSSSS7				1785					
280,000 TO	300,000	I 6SSSSSW3				1018					
300,000 TO	320,000	I ASSSSSSRF				768					
320,000 TO	340,000	I 5SSSSSSZ621				870					
340,000 TO	360,000	I BAYSSSSSSD1				474					
360,000 TO	380,000	I 15C0SSSSS91				371					
380,000 TO	400,000	I 2556I88334				241					
400,000 TO	420,000	I 14CALV881				188					
420,000 TO	440,000	I 235CBN81				97					
440,000 TO	460,000	I 139FN01				77					
460,000 TO	480,000	I 2668E1				30					
480,000 TO	500,000	I 53941				21					
500,000 TO	520,000	I 11661				14					
520,000 TO	540,000	I 11111				3					
540,000 TO	560,000	I 231				5					
560,000 TO	580,000	I 11				1					
580,000 TO	600,000	I + 1				1					
		SUMS									
		81	5								
		U26555544333222U									
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UNDER	IN	OVER	HMEAN =	=1,62268 IN	SIGMAN =	3,66881 IN
IN	2868	7737	VMEAN =	294,05753 GEV/C	SIGMAV =	93,27319 GEV/C
OVER	0	3	CORRELATION =	,91257		

TOTAL NUMBER OF PARTICLES CONSIDERED 11610

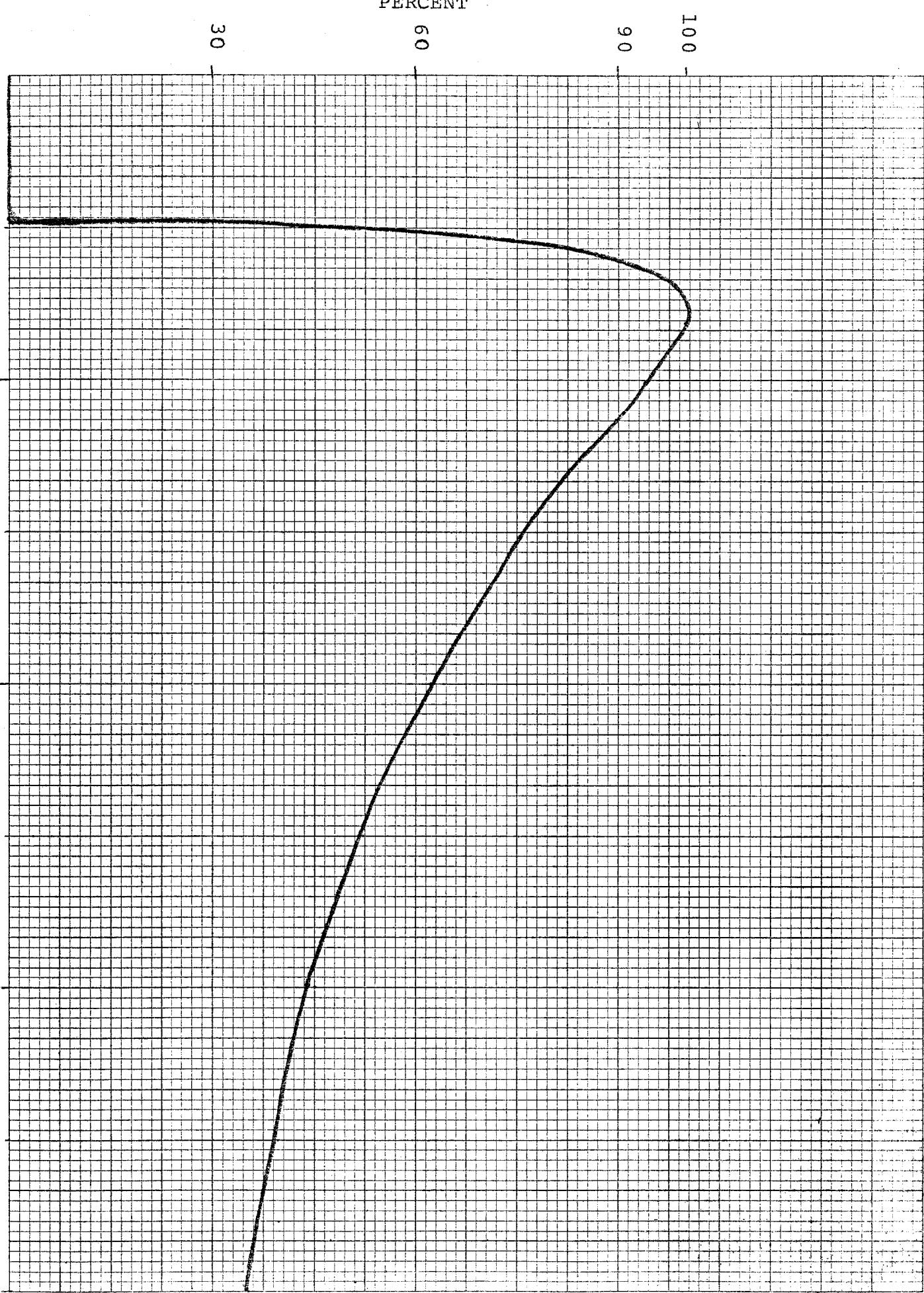
Beam 4 @ 305 GeV/c Tune

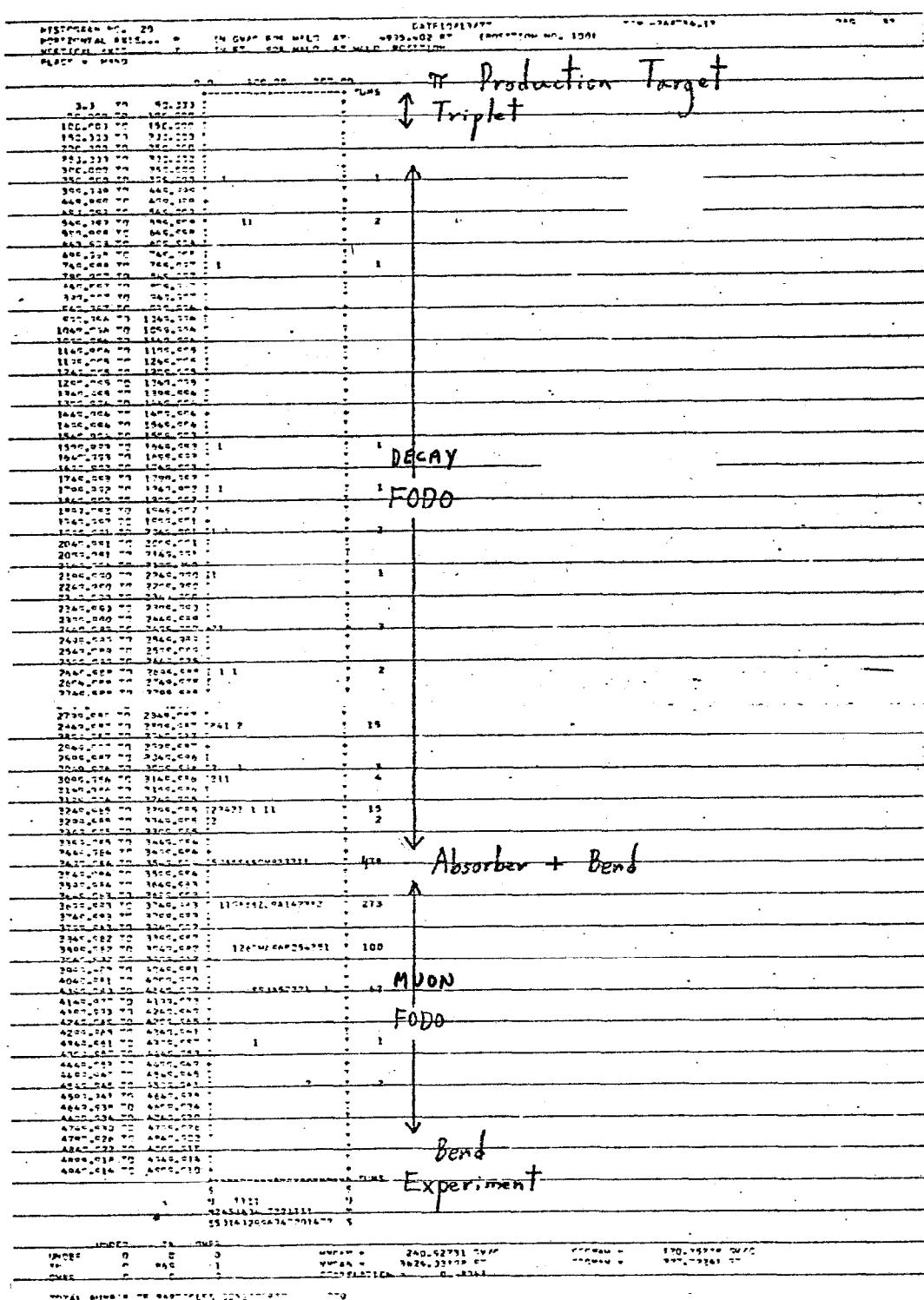
Dispersion at momentum slit

Fig. 3

FODO Transmission vs Momentum figure 4

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Longitudinal Points of Origin of Halo

Fig. 5

Plt = 13

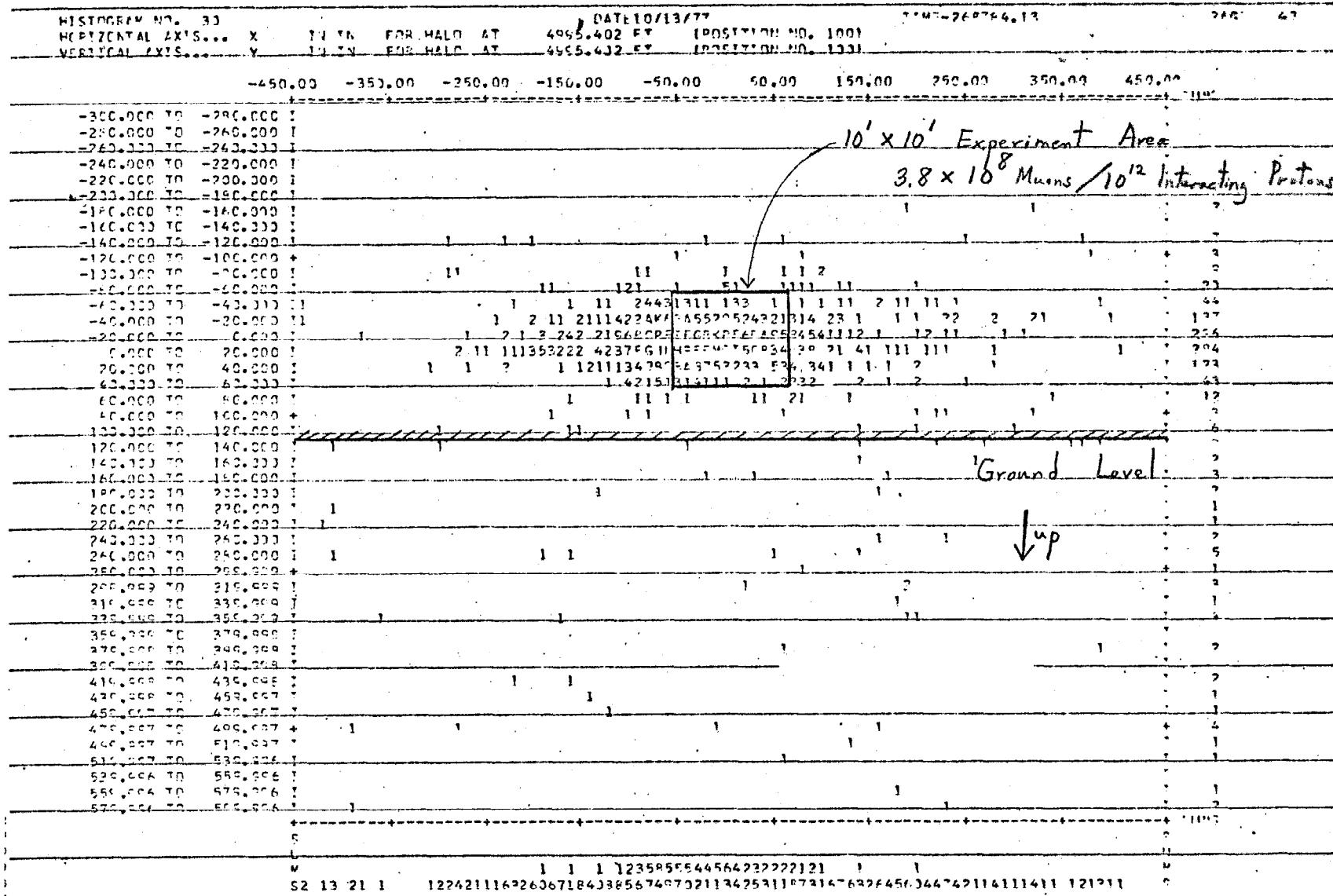


Fig. 6

1 Entry = 8.23×10^5 Muons / 10^{12} Protons

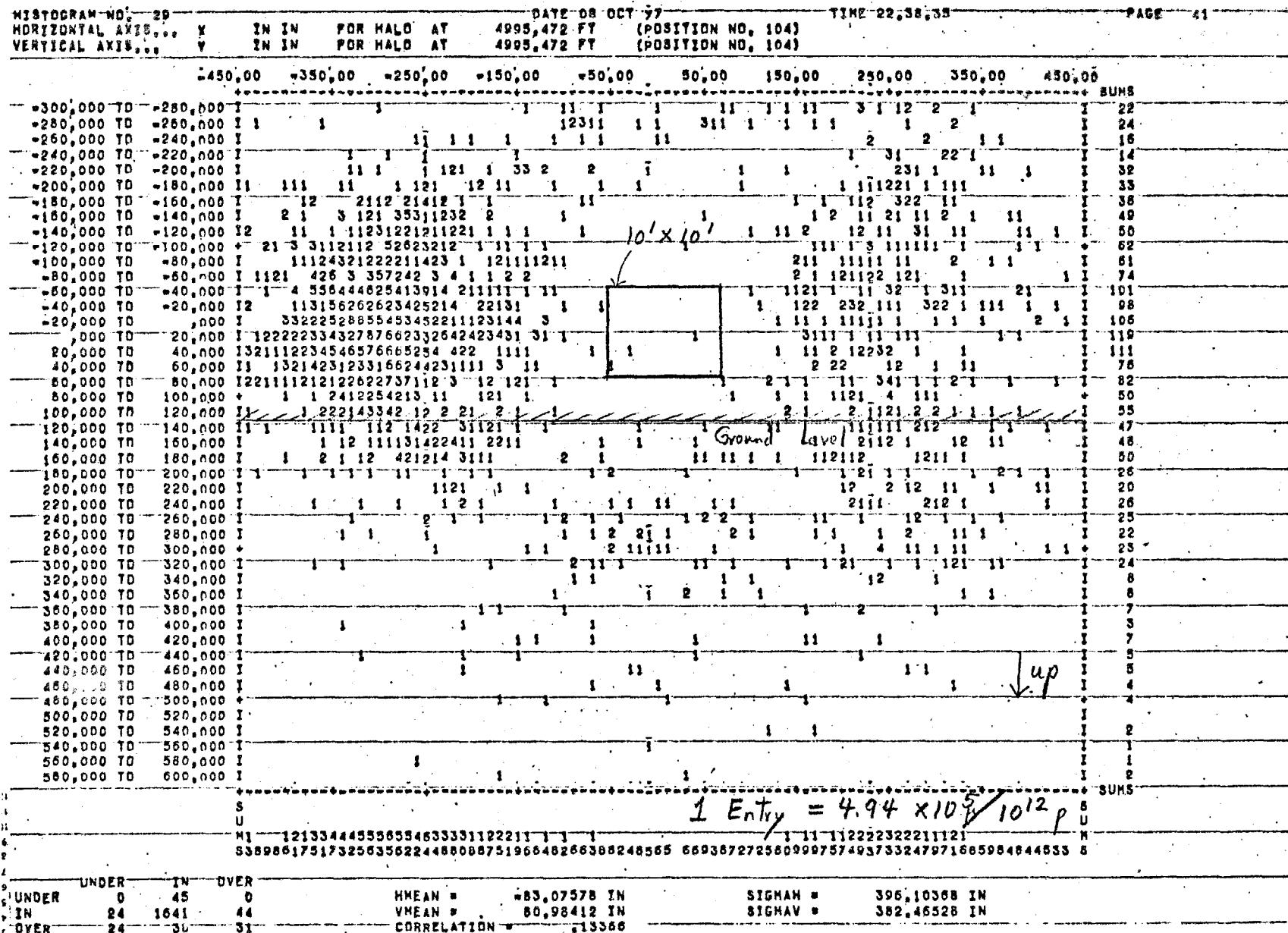


fig. 8a

BEAM 1

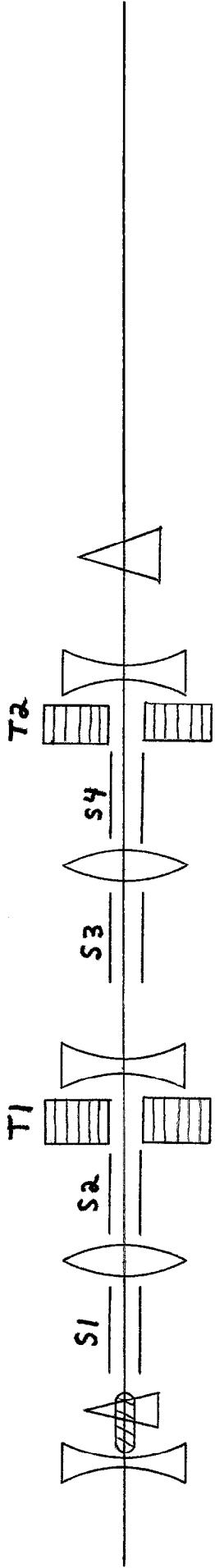


fig. 8b

BEAM 2 & 4

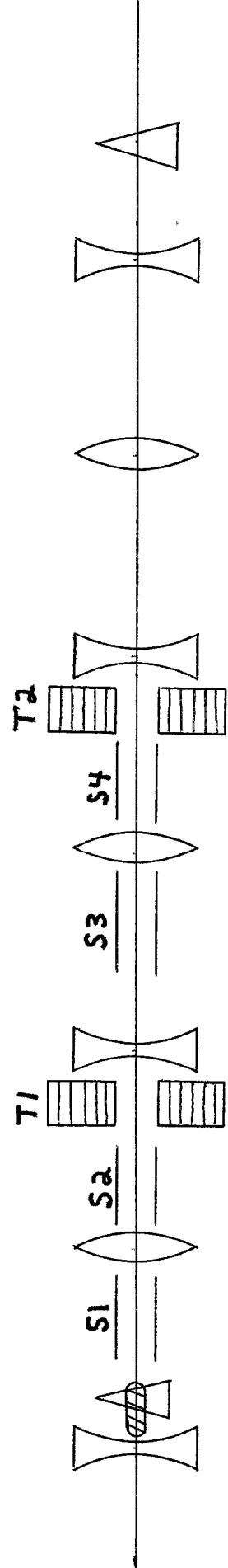
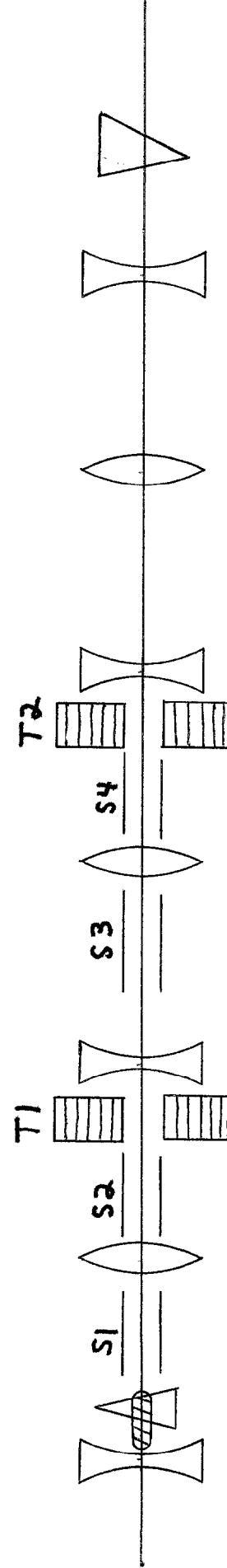


fig. 8c

BEAM 3



HISTOGRAM NO. 9			DATE 08 OCT 77	TIME 22:38:35	PAGE 20	
HORIZONTAL AXIS... COSTH IN FOR MU AT DECAY POSITION						
VERTICAL AXIS... P IN GEV/C FOR MU AT 4995.472 FT (POSITION NO. 104)						
			+1.00	0.00	-1.00	
					SUMS	
200,000	TO	220,000	I	I		
220,000	TO	240,000	I	I		
240,000	TO	260,000	I	I		
260,000	TO	280,000	I	I		
280,000	TO	300,000	I	I		
300,000	TO	320,000	I	I		
320,000	TO	340,000	I	I		
340,000	TO	360,000	I	11	2	
360,000	TO	380,000	I	I		
380,000	TO	400,000	I	11 11	5	
400,000	TO	420,000	I	11 11 11	8	
420,000	TO	440,000	I	1 2212 1 3141	17	
440,000	TO	460,000	I	3 11112 21 111211	16	
460,000	TO	480,000	I	111 111131125 2 311	25	
480,000	TO	500,000	I	2 1 113133423311	28	
500,000	TO	520,000	I	1 13213423131	24	
520,000	TO	540,000	I	1 11 12 22241	17	
540,000	TO	560,000	I	1 412112141121	22	
560,000	TO	580,000	I	1 221 11231	15	
580,000	TO	600,000	I	1111 2423 6	21	
600,000	TO	620,000	I	1 12 1 21	7	
620,000	TO	640,000	I	2 1 3		
640,000	TO	660,000	I	I		
660,000	TO	680,000	I	I		
680,000	TO	700,000	I	I		
700,000	TO	720,000	I	I		
720,000	TO	740,000	I	I		
740,000	TO	760,000	I	I		
760,000	TO	780,000	I	I		
780,000	TO	800,000	I	I		
					SUMS	
S					S	
U					U	
H					H	
S1422444384427899848						
UNDER	IN	OVER	HMEAN	,38782	SIGMAH	,45982
UNDER	0	0	VMEAN	,507,80819 GEV/C	SIGHAV	,61,38586 GEV/C
IN	0	211	CORRELATION	,22298		
OVER	0	0				
TOTAL NUMBER OF PARTICLES CONSIDERED			211			

Fig. 9

Beam 2

550 GeV/c

Pg. 29
TM-754
2900.00

HISTOGRAM NO. 8			DATE 09 OCT 77	TIME 13,15,35	PAGE 21
HORIZONTAL AXIS... COSTH IN FOR MU AT DECAY POSITION					
VERTICAL AXIS... IN GEV/C FOR MU AT 5025,972 FT (POSITION NO. 108)					
	-1.00	0.00	1.00		
			SUMS		
200,000 TD	220,000 I		I		
220,000 TD	240,000 I		I		
240,000 TD	260,000 I		I		
260,000 TD	280,000 I		I		
280,000 TD	300,000 I		I		
300,000 TD	320,000 I		I		
320,000 TD	340,000 I		I		
340,000 TD	360,000 I		I		
360,000 TD	380,000 I	I	I	2	
380,000 TD	400,000 I	I	I	3	
400,000 TD	420,000 I	I	I	14	
420,000 TD	440,000 I	I	I	10	
440,000 TD	460,000 I	I	I	22	
460,000 TD	480,000 I	I	I	47	
480,000 TD	500,000 I	I	I	51	
500,000 TD	520,000 I	I	I	65	
520,000 TD	540,000 I	I	I	94	
540,000 TD	560,000 I	I	I	103	
560,000 TD	580,000 I	I	I	96	
580,000 TD	600,000 I	I	I	88	
600,000 TD	620,000 I	I	I	55	
620,000 TD	640,000 I	I	I	19	
640,000 TD	660,000 I	I	I	10	
660,000 TD	680,000 I	I	I	1	
680,000 TD	700,000 I	I			
700,000 TD	720,000 I	I			
720,000 TD	740,000 I	I			
740,000 TD	760,000 I	I			
760,000 TD	780,000 I	I			
780,000 TD	800,000 I	I			
			SUMS		
	S	S			
U		I U			
M		I 1333455780RM			
S		I 13485867455382736328			
UNDER	0	0	OVER		
UNDER	0	0		HMEAN = .50204	SIGHAH = .39023
IN	0	580	0	VMEAN = 540.78180 GEV/C	SIGHAV = 53.44699 GEV/C
OVER	0	0	0	CORRELATION = .86090	
TOTAL NUMBER OF PARTICLES CONSIDERED	680				

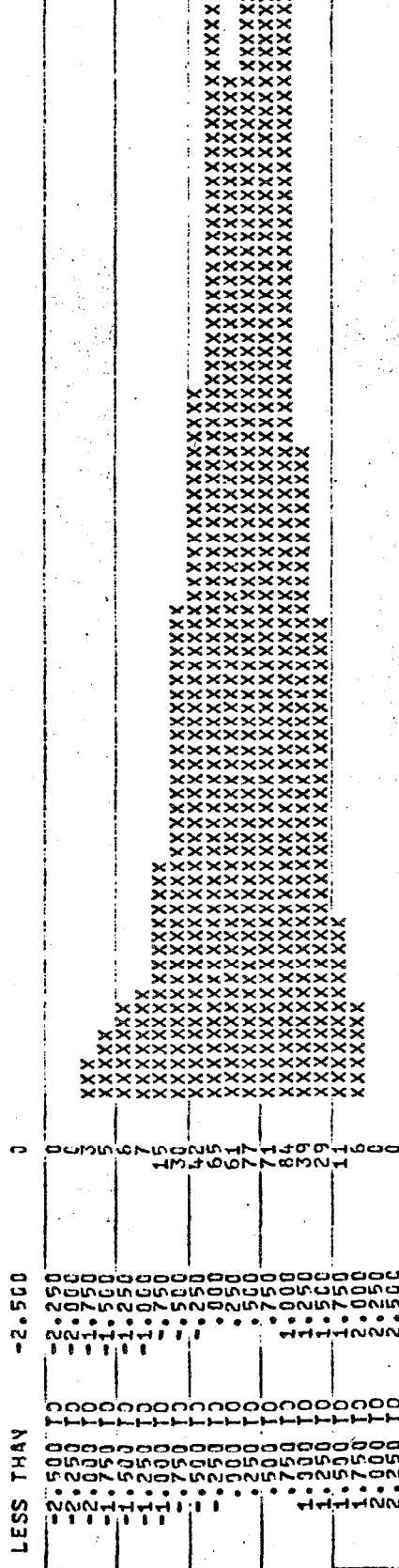
Fig. 10

Beam 4

550 GeV/c

HISTOGRAM NO. 7
DISTRIBUTION OF X IN IN FOR MU 4973.972 FT FROM THE TARGET

SCALE FACTOR = 100 X'S EQUAL 84 ENTRIES



TOTAL NUMBER OF ENTRIES = 551 INCLUDING UNDERFLOW AND OVERFLOW
CENTER = .329 RMS HALF-WIDTH = .698

HISTOGRAM NO. 7
DISTRIBUTION OF X IN IN FOR MU 4973.972 FT FROM THE TARGET

figure 11

HISTOGRAM NO 8

Y IN IN

FOR MU

4973.972 FT FROM THE TARGET

INTERVAL

SCALE FACTOR.. 100 X'S EQUAL 145 ENTRIES

LESS THAN -2.500 0

-2.500 TO -2.250	-2.250	0
-2.250 TO -2.000	-2.000	0
-2.000 TO -1.750	-1.750	0
-1.750 TO -1.500	-1.500	0
-1.500 TO -1.250	-1.250	0
-1.250 TO -1.000	-1.000	0
-1.000 TO -.750	-.750	18 XXX
-.750 TO -.500	-.500	31 XXXXXXXXXXXXXXXXX
-.500 TO -.250	-.250	86 XXXXXXXXXXXXXXXXXXXXXXXXX
-.250 TO .000	.000	145 XXXXXXXXXXXXXXXXXXXXXXXXX
.000 TO .250	.250	139 XXXXXXXXXXXXXXXXXXXXXXXXX
.250 TO .500	.500	73 XXXXXXXXXXXXXXXXXXXXXXXXX
.500 TO .750	.750	38 XXXXXXXXXXXXXXXXXXXXXXXXX
.750 TO 1.000	1.000	12 XXXXXXXX
1.000 TO 1.250	1.250	4 XX
1.250 TO 1.500	1.500	0
1.500 TO 1.750	1.750	0
1.750 TO 2.000	2.000	0
2.000 TO 2.250	2.250	0
2.250 TO 2.500	2.500	0

GREATER THAN 2.500 0

TOTAL NUMBER OF ENTRIES = 551 INCLUDING UNDERFLOW AND OVERFLOW
CENTER = -.010 RMS HALF WIDTH = .393

HISTOGRAM NO 8

Y IN IN

FOR MU

4973.972 FT FROM THE TARGET

figure 12

HISTOGRAM NO 10

P IN GEVC

FOR MU

4973.972 FT FROM THE TARGET

INTERVAL

SCALE FACTOR.. 100 X+S EQUAL 100 ENTRIES

LESS THAN 0.000

		0
0.000	TO	20.000
20.000	TO	40.000
40.000	TO	60.000
60.000	TO	80.000
80.000	TO	100.000
100.000	TO	120.000
120.000	TO	140.000
140.000	TO	160.000
160.000	TO	180.000
180.000	TO	200.000
200.000	TO	220.000
220.000	TO	240.000
240.000	TO	260.000
260.000	TO	280.000
280.000	TO	300.000
320.000	TO	340.000
340.000	TO	360.000
360.000	TO	380.000
380.000	TO	400.000
400.000	TO	420.000
420.000	TO	440.000
440.000	TO	460.000
460.000	TO	480.000
480.000	TO	500.000
500.000	TO	520.000
520.000	TO	540.000
540.000	TO	560.000
560.000	TO	580.000
580.000	TO	600.000
600.000	TO	620.000
620.000	TO	640.000
640.000	TO	660.000
660.000	TO	680.000
680.000	TO	700.000
700.000	TO	720.000
720.000	TO	740.000
740.000	TO	760.000
760.000	TO	780.000
780.000	TO	800.000
800.000	TO	820.000
820.000	TO	840.000
840.000	TO	860.000
860.000	TO	880.000
880.000	TO	900.000
900.000	TO	920.000
920.000	TO	940.000
940.000	TO	960.000
960.000	TO	980.000
980.000	TO	1000.000

GREATER THAN 1000.000

0

TOTAL NUMBER OF ENTRIES = 551 INCLUDING UNDERFLOW AND OVERFLOW
CENTER = 522.654 RMS HALF WIDTH = 43.623

APPENDIX I

The Parameters Used In HALO For The NI Beam

SYS DESCRIPTION	POSITION	TYPE	CODES	PARAMETERS	PAGE
NO. LENGTH					
1 0.0 FT	TUN	CIRC.	DIAF	36.000 IN 160.000 IN 0.0 IN 0.0 IN 0.0 DEG	2
	TUN			54.000 IN 160.000 IN 0.0 IN 0.0 IN 0.0 DEG	
1 0.0 FT	DRF			17.500 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
2 17.500 FT	APE CIRC	QUAD		1.500 IN 3.271 KG 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			10 10.000 FT 1.500 IN 0.0 IN 0.0 IN 0.0 DEG	
3 27.500 FT	DRF			1 1.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
4 29.500 FT	APE CIRC	QUAD		1.500 IN 3.271 KG 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			10 10.000 FT 1.500 IN 0.0 IN 0.0 IN 0.0 DEG	
5 39.500 FT	DRF			2 4.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
6 42.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
7 49.500 FT	DRF			1 1.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
8 50.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
9 57.500 FT	DRF			4 4.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
10 61.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
11 68.500 FT	DRF			1 1.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
12 69.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
13 76.500 FT	DRF			4 4.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
14 81.350 FT	APE QUAD			1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
15 88.390 FT	CRF			1 1.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
16 99.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
17 96.500 FT	CRF			1 3.000 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
18 99.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
19 106.500 FT	DRF			10 33.300 FT 0.0 IN 0.0 IN 0.0 IN 0.0 DEG	
20 119.500 FT	APE ELL	QUAD		1.000 IN 2.500 IN 0.0 IN 0.0 IN 0.0 DEG	
	QUAD Q310			7 7.000 FT 0.0 KG 1.000 IN 0.0 IN 0.0 IN 0.0 DEG	
21 146.500 FT					

SYS DESCRIPTION				DATE 9/20/77	TIME 268774.98	PAGE 4		
POSITION NO.	LENGTH	TYPE	CODES	PARAMETERS				
		1	2	3	4	5		
36	1561.394 FT	APE QUAD	CIRC. QUAD.	2.250 IN	0.0 IN	0.0 IN	0.0 DEG	
		QUAD Q610		10 10.000 FT	2,595 KG	2,500 IN		
37	1571.385 FT	JUN TUNO	CIRC ELL	4.000 IN	0.0 IN	0.3 IN	3.0 DEG	
				360.000 IN	252.000 IN	-156.000 IN	0.0 IN 0.0 DEG	
37	1571.385 FT	APE DRF	CIRC. DRF	6.000 IN	0.0 IN	0.3 IN	3.0 DEG	
		DRF		10 283.100 FT				
38	1854.485 FT	TUN TUNO	RECT ELL	60.000 IN	60.000 IN	0.0 IN	0.0 DEG	
				360.000 IN	252.000 IN	-180.000 IN	0.0 IN 0.0 DEG	
39	1854.485 FT	APE QUAD	ELL QDPB	2.500 IN	1.000 IN	0.0 IN	0.0 DEG	
		QUAD	QDPB	7 7.000 FT	3.975 KG	1.500 IN		
39	1861.485 FT	APE DRF	CIRC. DRF	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
		DRF		1 1.933 FT				
40	1863.385 FT	APE QUAD	ELL QDPB	2.500 IN	1.000 IN	0.0 IN	3.0 DEG	
		QUAD	QDPB	7 7.000 FT	3.975 KG	1.500 IN		
41	1970.385 FT	APE DRF	CIRC. DRF	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
		DRF		3 6.000 FT				
42	1876.384 FT	APE BEND	RECT M82	2.000 IN	1.000 IN	0.0 IN	0.0 DEG	
		BEND	M82	10 20.000 FT	7.845 KG	150.000 GV/C		
43	1896.384 FT	APE CRF	CIRC. DRF	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
		CRF		1 1.400 FT				
44	1957.784 FT	APE BEND	RECT M82	2.000 IN	1.000 IN	0.0 IN	0.0 DEG	
		BEND	M82	10 23.000 FT	7.845 KG	150.300 GV/C		
45	1917.784 FT	APE DRF	CIRC. DRF	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
		DRF		1 1.400 FT				
46	1919.184 FT	APS BEND	RECT M82	2.000 IN	1.000 IN	0.0 IN	0.0 DEG	
		BEND	M82	10 20.000 FT	7.845 KG	150.000 GV/C		
47	1939.183 FT	TUN TUNO	CIRC ELL	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
				360.000 IN	252.000 IN	-180.000 IN	0.0 IN 0.0 DEG	
47	1939.183 FT	APE CRF	CIRC. DRF	6.000 IN	0.0 IN	0.0 IN	0.0 DEG	
		CRF		10 371.666 FT				
48	2310.850 FT	TUN TUNO	RECT ELL	60.000 IN	60.000 IN	0.0 IN	0.0 DEG	
				360.000 IN	252.000 IN	-180.000 IN	0.0 IN 0.0 DEG	
48	2310.850 FT	APE ABS	CIRC. DRF POLY AIR	3.000 IN	3.0 IN	0.0 IN	0.0 DEG	
		DRF		5 20.000 FT				
49	2330.849 FT							

SYS DESCRIPTION				DATE 9/20/77	TIME 268774.58	PAGE 5		
POSITION NO.	TYPE	CODES	LENGTH	1	2	3	4	5
49	2330.849 FT	APE RECT BEND ABS RECT POLY FE BEND MB2	10	2.000 IN 2.000 IN 20.000 FT	1.000 IN 1.000 IN -7.751 KG	0.0 IN 3.0 IN 148.200 GV/C	0.0 IN 0.0 IN 0.0 DEG	0.0 IN 0.0 IN 0.0 DEG
50	2350.849 FT	APE CIRC DRF DRF	1	6.000 IN 1.400 FT		0.0 IN	0.0 IN	0.0 DEG
51	2352.249 FT	APE RECT BEND ABS RECT POLY FE BEND MB2	10	2.000 IN 2.000 IN 20.000 FT	1.000 IN 1.000 IN -7.688 KG	0.0 IN 0.0 IN 147.000 GV/C	0.0 IN 0.0 IN 3.0 DEG	0.0 DEG
52	2372.249 FT	APE CIRC DRF DRF	1	6.033 IN 1.400 FT		0.0 IN	0.0 IN	0.0 DEG
53	2373.649 FT	APE RECT BEND ABS RECT POLY FE BEND MB2	10	2.000 IN 2.000 IN 20.000 FT	1.000 IN 1.000 IN -7.625 KG	0.0 IN 0.0 IN 145.800 GV/C	0.0 IN 0.0 IN 3.0 DEG	0.0 DEG
54	2393.648 FT	TUN CIRC DIRT TUNG ELL		6.030 IN 480.000 IN	0.0 IN 252.000 IN	0.0 IN -240.000 IN	2.033 IN 0.0 IN	3.0 DEG 0.0 DEG
54	2393.648 FT	APE CIRC DRF DRF	10	6.000 IN 169.400 FT		0.0 IN	0.0 IN	0.0 DEG
55	2563.048 FT	TUN RECT DIRT TUVO ELL		60.000 IN 480.000 IN	60.000 IN 252.000 IN	0.0 IN -240.000 IN	0.0 IN 0.0 IN	0.0 DEG 3.0 DEG
55	2563.048 FT	APE CIRC QUAD QUAD Q610	4	6.000 IN 4.000 FT		0.0 IN 8.494 KG	0.0 IN 6.000 IN	0.0 DEG
56	2567.048 FT	APE CIRC DRF DRF	1	6.000 IN 2.000 FT		0.0 IN	3.0 IN	3.0 DEG
57	2569.048 FT	APE CIRC QUAD QUAD Q610	4	6.000 IN 4.000 FT		3.0 IN 8.494 KG	0.0 IN 6.000 IN	3.0 DEG
58	2573.049 FT	APE CIRC DRF CRF	1	6.000 IN 2.200 FT		0.0 IN	0.0 IN	0.0 DEG
59	2575.248 FT	APE CIRC QUAD QJ0 Q610	6	6.000 IN 4.000 FT		0.0 IN 8.494 KG	0.0 IN 6.000 IN	0.0 DEG
60	2579.248 FT	APE CIRC DRF DRF	1	6.000 IN 16.733 FT		0.0 IN	0.0 IN	0.0 DEG
61	2595.948 FT	APE CIRC QUAD QUAD Q610	4	6.000 IN 4.000 FT		0.0 IN -8.494 KG	0.0 IN 6.000 IN	0.0 DEG
62	2599.947 FT	APE CIRC DRF DRF	1	6.033 IN 1.900 FT		3.0 IN	0.0 IN	0.0 DEG
63	2601.847 FT							

SYS DESCRIPTION.		DATE 9/20/77		TIME 268774.00		PAGE 6	
POSITION NO.	TYPE	CODES		PARAMETERS			
		1	2	3	4	5	
63	2601.847 FT	APE QUAD	CIRC 0610	4 6.000 IN 4.000 FT	-8.494 KG	0.0 IN 6.000 IN	0.0 IN 0.0 DEG
64	2605.947 FT	APE DRF	CIRC DRF	4 6.000 IN 1 2.200 FT		0.0 IN	0.0 IN 0.0 DEG
65	2608.047 FT	APE QUAD	CIRC QUAD	4 6.000 IN 4.000 FT	-8.494 KG	0.0 IN 6.000 IN	0.0 IN 0.0 DEG
66	2612.047 FT	TUN TUNO	CIRC ELL	6.000 IN \$40.000 IN	252.000 IN	0.0 IN -300.000 IN	2.000 IN 0.0 IN 0.0 DEG
66	2612.047 FT	APE DRF	CIRC DRE	6.000 IN 10 233.600 FT		0.0 IN	0.0 IN 0.0 DEG
67	2845.646 FT	TUN TUNO	RECT ELL	60.000 IN 610.000 IN	60.000 IN 252.000 IN	0.0 IN -480.000 IN	0.0 IN 0.0 IN 3.0 DEG
67	2845.646 FT	APE BEND	RECT BEND	2.000 IN 10 23.000 FT	1.500 IN 7.594 KG	0.0 IN 145.230 GV/C	0.0 IN 0.0 DEG
68	2865.646 FT	APE DRF	CIRC DRF	6.000 IN 1 1.500 FT		0.0 IN	0.0 IN 0.0 DEG
69	2867.146 FT	APE BEND	RECT MB3	2.000 IN 10 20.000 FT	1.530 IN 7.594 KG	0.0 IN 145.200 GV/C	0.0 IN 0.0 DEG
70	2887.146 FT	APE DRF	CIRC DRF	6.000 IN 1 1.200 FT		0.0 IN	0.0 IN 0.0 DEG
71	2888.346 FT	APE BEND	RECT MB3	2.000 IN 10 20.000 FT	1.500 IN 7.594 KG	0.0 IN 145.200 GV/C	0.0 IN 0.0 DEG
72	2908.345 FT	TUN TUNO	CIRC ELL	6.000 IN 610.000 IN	252.000 IN	0.0 IN -480.000 IN	2.000 IN 0.0 IN 0.0 DEG
72	2908.345 FT	APE CRF	CIRC DRF	6.000 IN 5 85.500 FT		0.0 IN	0.0 IN 0.0 DEG
73	2993.845 FT	TUN TUNO	RECT AIR	360.000 IN 361.000 IN	120.000 IN 121.000 IN	120.000 IN 120.000 IN	60.000 IN 60.000 IN 0.0 DEG
73	2993.845 FT	APE DRF	CIRC DRF	6.000 IN 2 20.000 FT		0.0 IN	0.0 IN 0.0 DEG
74	3013.845 FT	APE COLL	RECT DRF	6.000 IN 100.000 IN	4.000 IN 50.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 DEG
75	3016.845 FT	APE DRF	RECT DRF	1 3.000 FT		0.0 IN	0.0 IN 0.0 DEG
76	3019.845 FT	APE DRF	RECT DRF	1 3.000 FT		0.0 IN	0.0 IN 0.0 DEG

SYS DESCRIPTION..... DATE 9/23/73 .. TIME 260774.98 PAGE 7

POSITION NO.	TYPE	CODES	PARAMETERS
		1 2 3	1 2 3 4 5
76 3019.845 FT	APE - RECT - BEND	72.003 IN 18.000 IN 0.0 IN 0.0 DEG	
	BEND MB36'	2 13.300 FT 14.920 KG 145.200 GV/C	
77 3033.145 FT	APE - RECT - DRF	6.000 IN 4.000 IN 1.C.O. IN 0.0 IN 0.0 DEG	
	DRF	2 26.600 FT	
78 3059.745 FT			

APPENDIX II

The Parameters Used in HALO For The Four Doubler Muon Beams

MUCH CF NEUTRINO BEAM.
 MUCH MOMENTUM 0.0 TC 1000,000 EV/C
 IN THE HISTOGRAMS BELOW, ENTRY REPRESENTS .0.14814E-07 MUCNS CR. NEUTRINOS

SYS DESCRIPTION.			DATE 9/22/77		TIME-268780.94			PAGE 3	
POSITION NO.	LENGTH	TYPE	CODES			PARAMETERS			5
			1	2	3	1	2	3	
21	142.472 FT	DRF				1	1.500 FT		
22	143.572 FT	DRF	APE QUAD	CIRC Q410	QUAD	5	2.250 IN 10.000 FT	-1.341 KG 1.000 IN	0.0 IN 0.0 DEG
23	153.672 FT	DRF	BEND			3	14.500 FT		
24	168.472 FT	DRF	APE BEND	RECT MB6	BEND	5	3.000 IN 20.000 FT	2.000 IN -11.250 KG	0.0 IN 600.000 GV/C
25	188.472 FT	DRF				8	45.000 FT		
26	233.472 FT	DRF	APE BEND	RECT MB6	BEND	5	3.000 IN 20.000 FT	2.000 IN 11.250 KG	-1.003 IN 600.000 GV/C
27	253.472 FT	DRF				1	1.300 FT		
28	254.472 FT	DRF	APE BEND	RECT MB6	BEND	5	3.000 IN 20.000 FT	2.003 IN 11.250 KG	-1.300 IN 600.000 GV/C
29	274.471 FT	DRF				8	45.000 FT		
30	310.471 FT	DRF	APE BEND	RECT MB6	BEND	5	3.000 IN 20.000 FT	2.000 IN -11.250 KG	0.0 IN 600.000 GV/C
31	339.471 FT	DRF				3	14.500 FT		
32	353.471 FT	DRF	APE QUAD	CIRC Q410	QUAD	5	2.250 IN 10.000 FT	0.0 IN 2.682 KG	0.0 IN 1.000 IN
33	363.970 FT	DRF				2	10.000 FT		
34	373.570 FT	DRF	APE COLL	CIRC RECT	DRF VAC	4	4.000 IN 900.000 IN	0.0 IN 900.000 IN	0.0 IN -750.000 IN
			DIRT			5	900.000 IN 190.000 FT	0.0 IN -2.692 KG	0.0 IN 1.000 IN
35	543.970 FT	DRF	APE QUAD	CIRC Q410	QUAD	2	2.250 IN 10.000 FT	0.0 IN -2.692 KG	0.0 IN 1.000 IN
36	573.970 FT	DRF	APE CPE	CIRC DPF	DPF	4	4.000 IN 190.000 FT	0.0 IN 900.000 IN	0.0 IN -750.000 IN
37	583.569 FT	DRF	APE COLL	CIRC RECT	DRF VAC	5	4.000 IN 900.000 IN	0.0 IN 900.000 IN	0.0 IN -750.000 IN
			DIRT			10	900.000 IN 190.000 FT	0.0 IN -2.692 KG	0.0 IN 1.000 IN
38	773.569 FT	DRF	APE QUAD	CIRC Q410	QUAD	2	2.250 IN 10.000 FT	0.0 IN 2.682 KG	0.0 IN 1.000 IN
39	783.969 FT	DRF	APE DRF	CIRC DPF	DPF	4	4.000 IN 10.000 FT	0.0 IN -2.692 KG	0.0 IN 0.0 DEG
40	793.969 FT					5	10.000 FT		

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NO.	POSITION LENGTH	TYPE	CODES			PARAMETERS			3	4
				1	2	3	4	5		
43	751.969 FT	APE COLL DRF	CIRC RECT VAC	DIRT	4.000 IN 900.000 IN 190.000 FT	900.000 IN	0.0 IN 0.0 IN -790.000 IN	0.0 IN 0.0 DEG 0.0 DEG		
41	983.969 FT	APE QUAD	CIRC Q410		2.250 IN 5 10.000 FT	-2.682 KG	0.0 IN 1.000 IN	0.0 IN 0.0 DEG		
42	993.968 FT	APE DRF	CIRC		4.000 IN 2 10.000 FT		0.0 IN	0.0 IN 0.0 DEG		
43	1003.968 FT	APE COLL DRF	CLOC RECT VAC	DIRT	4.000 IN 903.000 IN 190.000 FT	900.000 IN	0.0 IN 0.0 IN -780.000 IN	0.0 IN 0.0 DEG 0.0 DEG		
44	1193.968 FT	APE QUAD	CIRC Q410	QUAD	2.250 IN 5 10.000 FT	2.682 KG	0.0 IN 1.000 IN	0.0 IN 0.0 DEG		
45	1203.968 FT	APE DRF	CIRC	DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN 0.0 DEG		
46	1213.967 FT	APE COLL DRF	CIRC RECT VAC	DIRT	4.000 IN 900.000 IN 190.000 FT	900.000 IN	0.0 IN 0.0 IN -780.000 IN	0.0 IN 0.0 DEG 0.0 DEG		
47	1403.967 FT	APE QUAD	CIRC Q410	QUAD	2.250 IN 5 10.000 FT	-2.682 KG	0.0 IN 1.000 IN	0.0 IN 0.0 DEG		
48	1413.967 FT	APE DRF	CIRC	DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN 0.0 DEG		
49	1423.967 FT	APE COLL DRF	CIRC RECT VAC	DIRT	4.000 IN 900.000 IN 190.000 FT	900.000 IN	0.0 IN 0.0 IN -780.000 IN	0.0 IN 0.0 DEG 0.0 DEG		
50	1613.966 FT	APE QUAD	CIRC Q410	QUAD	2.250 IN 5 10.000 FT	2.682 KG	0.0 IN 1.000 IN	0.0 IN 0.0 DEG		
51	1623.966 FT	APE DRF	CIRC	DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN 0.0 DEG		
52	1633.966 FT	APE COLL DRF	CIRC RECT VAC	DIRT	4.000 IN 900.000 IN 190.000 FT	900.000 IN	0.0 IN 0.0 IN -780.000 IN	0.0 IN 0.0 DEG 0.0 DEG		
53	1823.966 FT	APE QUAD	CIRC Q410	QUAD	2.250 IN 5 10.000 FT	-2.682 KG	0.0 IN 1.000 IN	0.0 IN 0.0 DEG		
54	1833.965 FT	APE DRF	CIRC	DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN 0.0 DEG		
55	1843.965 FT	APE COLL DRF	CIRC RECT VAC	DIRT	4.000 IN 903.000 IN 190.000 FT	903.000 IN	0.0 IN 0.0 IN -780.000 IN	0.0 IN 0.0 DEG 0.0 DEG		

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NO.	POSITION LENGTH	TYPE	CNODES	1	2	3	4	1	2	3	4	5	1	2	3
56	2033.965 FT	APE CIRC QUAD Q410	4	2.250 IN	-10.000 FT	2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
57	2343.965 FT	APE CIRC DRF Q4F	2	4.000 IN	10.000 FT		0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
58	2353.964 FT	APE CIRC DRF CCFL SECT VAC DIST	10	4.000 IN	933.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG					
59	2263.964 FT	APE CIRC QUAD QUAD Q410	5	2.250 IN	10.000 FT	-2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
60	2253.964 FT	APE CIRC DAE CRF	2	4.000 IN	10.000 FT		0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
61	2263.964 FT	APE CIRC DSE CCFL RECT VAC DIST	10	4.000 IN	933.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG					
62	2451.963 FT	APE CIRC Q410	5	2.250 IN	10.000 FT	2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
63	2463.963 FT	APE CIRC DRF CCFL DRF	2	4.000 IN	10.000 FT		0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
64	2471.963 FT	APE CIRC DRF CCFL VAC DIST	10	4.000 IN	933.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG					
65	2663.963 FT	APE CIRC DRF CCFL Q410	5	2.250 IN	10.000 FT	-2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
66	2673.962 FT	APE CIRC DRF CCFL SECT VAC DIST	10	4.000 IN	10.000 FT		0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
67	2683.962 FT	APE CIRC DRF CCFL Q410	5	2.250 IN	10.000 FT	2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
68	2873.962 FT	APE CIRC DRF CCFL SECT VAC DIST	10	4.000 IN	933.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG					
69	2883.962 FT	APE CIRC DRF CCFL Q4F	2	4.000 IN	10.000 FT	-2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
70	2893.961 FT	APE CIRC DRF CCFL VAC DIST	10	4.000 IN	900.000 IN	400.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
71	3003.961 FT	APE CIRC QUAD Q410	5	2.250 IN	10.000 FT	-2.682 KG	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 DEG				
72	3053.961 FT	APE CIRC DRF CCFL VAC DIST	10	4.000 IN	900.000 IN	-780.000 IN	0.0 IN	0.0 IN	0.0 IN	0.0 IN	0.0 NEG				

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POSITION NO.	LENGTH	TYPE	CODES			PARAMETERS		
			1 2 3	1	2	3	4	5
72	3093.961 FT	APE DRF	CIRC VAC	4.000 IN 10.000 FT		0.0 IN	0.0 IN	0.0 DEG
73	3103.961 FT	APE COLL DRF	CIRC RECT VAC	4.000 IN .900.000 IN 10 190.000 FT	900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG 0.0 DEG
74	3293.960 FT	APE QDAD	CIRC 0410	2.250 IN 10.000 FT	2.682 KG	0.0 IN 1.000 IN	0.0 IN	0.0 DEG
75	3303.960 FT	APE CRF	CIRC DRF	4.000 IN 10.000 FT		0.0 IN	0.0 IN	0.0 DEG
76	3313.960 FT	APE COLL CRF	CIRC RECT VAC	4.000 IN 900.000 IN 10 190.000 FT	900.000 IN	0.0 IN 0.0 IN	-3.0 IN -780.000 IN	0.0 DEG 0.0 DEG
77	3503.962 FT	APE ABS QUAD	CIRC 9E 2410	2.250 IN 2.250 IN 10.000 FT	-2.458 KG	0.0 IN 0.0 IN 1.000 IN	0.0 IN 0.0 IN	0.0 DEG 0.0 DEG
78	3513.959 FT	APE ABS CRF	CIRC RECT BE	3.000 IN 60.000 IN 5 1.500 FT		0.0 IN 0.0 IN	0.3 IN 0.0 IN	0.0 DEG 0.0 DEG
79	3515.959 FT	APE ABS BEND	RECT BE BE	3.000 IN 3.000 IN 5 20.000 FT	2.000 IN 2.000 IN 11.000 KG	0.0 IN 0.3 IN 550.000 GV/C	0.0 IN 0.0 IN	0.0 DEG 0.0 DEG
80	3535.959 FT	APE COLL CRF	CIRC RECT VAC	4.000 IN 900.000 IN 3 28.500 FT	900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG 0.0 DEG
81	3563.959 FT	TIN TUNU	CIRC RECT	3.000 IN 900.000 IN	900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG 0.0 DEG
81	3563.959 FT	APE SCR	CIRC SCR	2.000 IN 150.000 FT		0.0 IN 0.0 IN	0.3 IN 2.000 IN	0.0 DEG 3.000 IN
82	3713.958 FT	TIN TUNU	RECT RECT	60.000 IN 500.000 IN	48.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG 0.0 DEG
82	3713.959 FT	APE QUAD	CIRC 0410	2.250 IN 10.000 FT		0.0 IN 2.458 KG	0.0 IN 1.000 IN	0.0 DEG
83	3723.958 FT	APE CRE	CIRC DRF	4.000 IN 10.000 FT		0.0 IN	0.0 IN	0.0 DEG
84	3733.958 FT	TIN TUNU	CIRC RECT	3.000 IN 900.000 IN	900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG 0.0 DEG
84	3733.958 FT							

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POSIT'N	TYPE	CODES	PARAMETERS	1	2	3	4	1	2	3	4	1	2	3	4
NC.	LENGTH														
84	3713.556 FT	APE CIRC SCR	2.000 IN 15.000 FT	2.000 IN 15.000 KG	0.0 IN 0.0 IN	0.0 IN 0.0 IN	3.0 DEG	3.0 DEG	3.000 IN	3.000 IN	3.000 IN	3.0 DEG	3.0 DEG	3.0 DEG	3.0 DEG
85	3883.750 FT	TUN CIRC DIRT	60.000 IN 900.000 IN	60.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
85	3883.558 FT	APE CIRC SCR	3.000 IN 40.000 FT	3.000 IN 40.000 KG	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	3.000 IN	3.000 IN	3.000 IN	0.0 DEG	3.000 IN	3.000 IN	0.0 DEG
86	3923.556 FT	TUN RECT DIRT	60.000 IN 900.000 IN	48.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
86	3923.556 FT	TUN RECT	900.000 IN 900.000 IN	900.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	780.000 IN	780.000 IN	780.000 IN	0.0 DEG	780.000 IN	780.000 IN	0.0 DEG
87	3933.957 FT	APE CIRC QUAD	2.250 IN 10.000 FT	2.458 IN 10.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	1.000 IN	1.000 IN	1.000 IN	0.0 DEG	1.000 IN	1.000 IN	0.0 DEG
88	3943.957 FT	APE CIRC DRF	4.000 IN 10.000 FT	4.333 IN 10.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
89	3953.457 FT	COLL REC VAC	900.000 IN 43.000 FT	900.000 IN 43.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	740.000 IN	740.000 IN	740.000 IN	0.0 DEG	740.000 IN	740.000 IN	0.0 DEG
89	3953.457 FT	TUN CIRC DIRT	3.000 IN 900.000 IN	3.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
89	3983.557 FT	APE CIRC SCR	2.000 IN 15.000 FT	1.5000 IN 15.000 KG	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	780.000 IN	780.000 IN	780.000 IN	0.0 DEG	780.000 IN	780.000 IN	0.0 DEG
90	4133.553 FT	TUN RECT DIRT	60.000 IN 900.000 IN	48.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
90	4133.553 FT	TUN RECT	900.000 IN 900.000 IN	900.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	780.000 IN	780.000 IN	780.000 IN	0.0 DEG	780.000 IN	780.000 IN	0.0 DEG
91	4143.445 FT	APE CIRC QUAD	2.250 IN 10.000 FT	2.458 IN 10.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	1.000 IN	1.000 IN	1.000 IN	0.0 DEG	1.000 IN	1.000 IN	0.0 DEG
92	4153.445 FT	CRF APE CIRC DSE	4.000 IN 12.000 FT	4.000 IN 12.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
92	4153.445 FT	TUN CIRC DIRT	3.000 IN 900.000 IN	3.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
92	4153.445 FT	APE CIRC SCR	2.000 IN 15.000 FT	1.5000 IN 15.000 KG	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
93	4303.941 FT	TUN CIRC DIRT	40.000 IN 900.000 IN	900.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
93	4303.941 FT	APE CIRC SCR	1.000 IN 40.000 FT	1.5000 IN 40.000 FT	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG
94	4343.718 FT	TUN SECT CIRZ	60.000 IN 900.000 IN	48.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	740.000 IN	740.000 IN	740.000 IN	0.0 DEG	740.000 IN	740.000 IN	0.0 DEG
94	4343.718 FT	TUN RECT	900.000 IN 900.000 IN	900.000 IN 900.000 IN	0.0 IN 0.0 IN	0.0 IN 0.0 IN	0.0 DEG	0.0 DEG	0.0 IN	0.0 IN	0.0 IN	0.0 DEG	0.0 IN	0.0 IN	0.0 DEG

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POSITION NO.	TYPE LNGTH	CODES	1	2	3	4	5	
94 4343.938 FT	APE QUAD	CIRC QUAD	2.250 IN 5 10.000 FT	-2.458 KG	0.0 IN 1.000 IN	0.0 IN	0.0 DEG	
95 4353.934 FT	APE CRF	CIRC DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN	0.0 DEG	
96 4363.933 FT	APE COLL CPF	CIRC DRF RECT VAC	4.000 IN DIRT 900.000 IN 10 190.000 FT	900.000 IN	0.0 IN C.C. IN	0.0 IN -780.000 IN	0.0 DEG	
97 4553.926 FT	APE QUAD	CIRC QUAD	2.250 IN 5 10.000 FT	2.458 KG	0.0 IN 1.000 IN	0.0 IN	0.0 DEG	
98 4563.922 FT	APE CRF	CIRC DRF	4.000 IN 2 10.000 FT		0.0 IN	0.0 IN	0.0 DEG	
99 4573.918 FT	APE COLL DRF	CIRC DRF	4.000 IN RECT VAC	900.000 IN	0.0 IN 0.3 IN	0.0 IN -780.000 IN	0.0 DEG	
100 4763.916 FT	APE QUAD	CIRC QUAD	2.250 IN 5 10.000 FT	-2.458 KG	0.0 IN 1.000 IN	0.0 IN	0.0 DEG	
101 4773.912 FT	APE COLL DRF	CIRC DRF	4.000 IN RECT VAC	900.000 IN	0.0 IN 0.3 IN	0.0 IN -780.000 IN	0.0 DEG	
102 4863.906 FT	APE BEND	RECT RFND	3.000 IN 5 20.000 FT	2.000 IN 11.000 KG	0.3 IN 550.000 GV/C	0.3 IN	0.0 DEG	
103 4883.902 FT	APE COLL DRF	CIRC DRF	4.000 IN RECT VAC	900.000 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG	
104 4993.902 FT	APE COLL DRF	CIRC DRF	0.0 IN RECT VAC	8999.996 IN	0.0 IN 0.0 IN	0.0 IN -780.000 IN	0.0 DEG	
105 51555.355 FT				10 6599.996 FT				

APPENDIX III

PROPERTIES OF THE MUPPIPE

A) Magnetic Field

Using $\oint \vec{H} \cdot d\vec{s} = I$ we obtain

$$\vec{H}(r) = 0 \quad r < a$$

$$\vec{H}(r) = \frac{I}{2\pi r} \hat{\theta} \quad r > b$$

$$\vec{H}(r) = \frac{I(r^2 - a^2)}{2\pi r(b^2 - a^2)} \hat{\theta} \quad a < r < b$$

$$\vec{B}(r) = \mu(H) \vec{H}$$

Of primary interest is the region $a < r < b$. Figures A1 and A2 show the relevant quantities for pure iron and for hot rolled low-carbon steel.

(See reference 11). The parameters were $I=5000$ amps, $a=2$ inches, and $b=3$ inches. $d=r-a$. In both pure iron and hot rolled steel, the magnetic field attains very high values after only penetrating a small distance into the mupipe wall.

B. Power (D. C.)

$$P = I^2 R = \frac{I^2 L}{\pi(b^2 - a^2)}$$

Using $\rho = 1.6 \times 10^{-5}$ cm, we obtain

$$\frac{P}{L} = 4 \text{ watts/cm} = 122 \text{ watts/foot}$$

C) Deflection in pure iron

$$p_{\text{LMS}} = 0.15 \sqrt{\frac{L}{0.0176 \text{ m}}} = 0.113 \sqrt{L} \text{ GeV/c (meters)}^{-1/2}$$

$$p_{\text{LB}} = 0.03BL$$

$$T = \frac{p_{\text{LB}}}{p_{\text{LMS}}} = \frac{0.03BL}{0.113\sqrt{L}} = 0.265B\sqrt{L} \text{ kg}^{-1} \text{ meters}^{-1/2}$$

At what angle does a particle have to enter the wall of the mupipe so that L is large enough for $p_{\text{LB}} > p_{\text{LMS}}$? For a particle that enters the wall at an angle θ , $L(\theta)$ can be found from:

$$L^2 = 2\rho^2\theta^2 + 2\rho d - \rho d\theta^2 - 2\rho\theta\sqrt{\rho^2\theta^2 + 2\rho d - d^2 - \rho d\theta^2}$$

ρ = the radius of curvature

d = depth into the wall

For a particle that overcomes multiple scattering, the average B field is 16.7 kg and calculating L, gives L=9 meters for $p = 800 \text{ GeV/c}$, and L=3 meters for $p=100 \text{ GeV/c}$. Figure A3 shows T vs L for several angles and indicates that the field wins over the multiple scattering at $\sim 0.008 \text{ mr}$ for $p=800 \text{ GeV/c}$, and at $\sim 0.03 \text{ mr}$ for $p=100 \text{ GeV/c}$.

figure A1

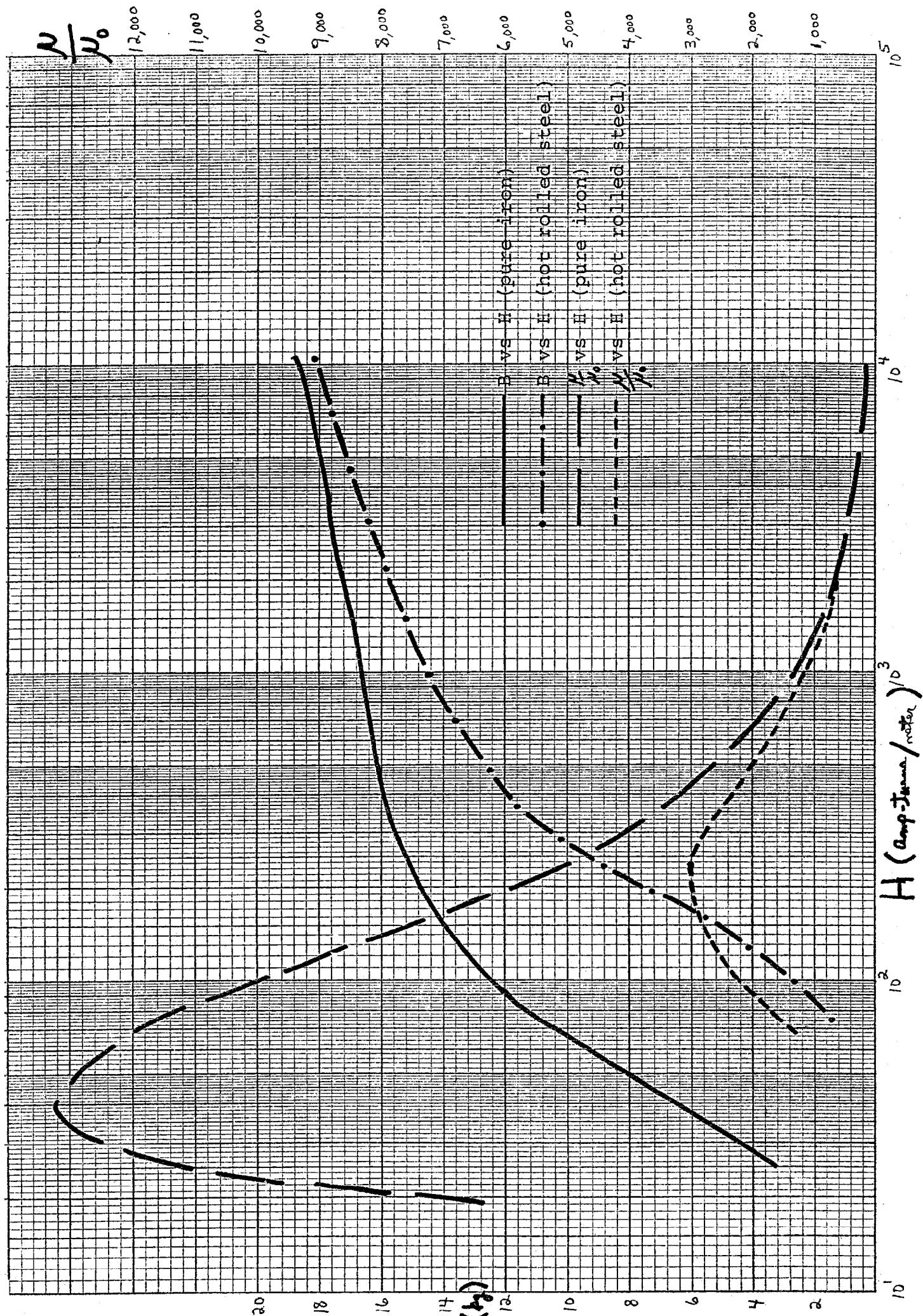
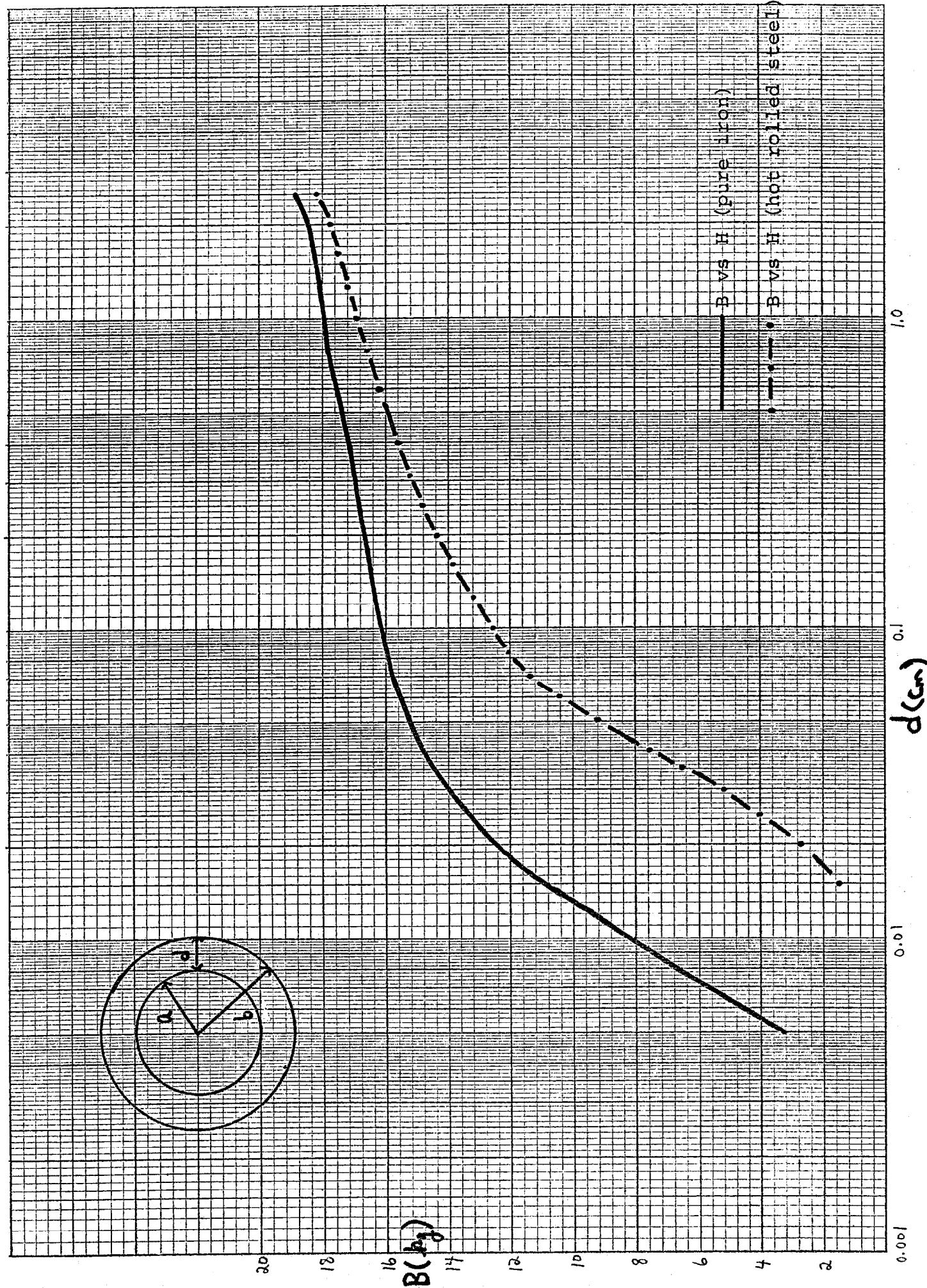


figure A2

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figure A3

